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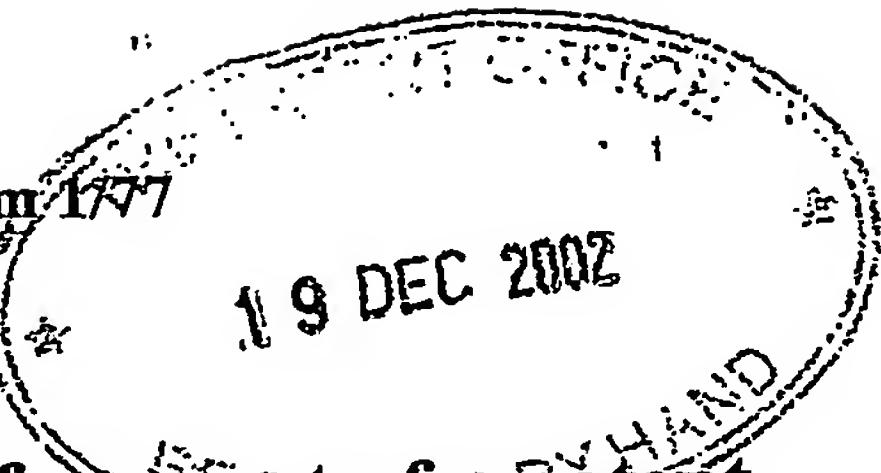
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NJH/FP5985908

19 DEC 2002

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Patents ADP number (if you know it)

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If the applicant is a corporate body, give the country/state of its incorporation

4. Title of the invention

AN OPTICAL FILTER

5. Name of your agent (if you have one)

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An Optical Filter

The present invention relates to optical filters in the  
5 form of optical coatings applied to substrates. The  
present invention relates particularly, though not  
exclusively, to optical filters for photovoltaic cells,  
especially solar cells.

10 Photovoltaic cells, such as solar cells, typically  
possess a preferential optical operating spectrum  
across/within which it is desired to have the  
photovoltaic cell operate. This may be because the  
design of the cell causes it to be relatively efficient  
15 in respect of, or to be relatively sensitive to, optical  
radiation within such a preferential spectrum.

Alternatively, or additionally, it may be the case that  
optical radiation outside the operating spectrum is in  
some way detrimental to the operation of the cell.

20 For example, the efficiency of the photo-electrical  
conversion process of many photovoltaic cells falls as  
the temperature of the cell rises. Consequently, many  
solar cells employ filters designed to exclude from  
25 radiation incident upon the cell those wavelengths of  
radiation which have a propensity to heat the cell.

Typically, the filters are designed to reflect incident Infra-Red (IR) radiation. Other filters designed to exclude other types of optical radiation, such as Ultra-Violet (UV) radiation which may be damaging to certain components of the solar cell, may be employed. These other filters may be separate from the IR type filters. Alternatively, a single "band-pass" filter may be employed which is designed to simultaneously exclude not only IR radiation but also UV radiation from radiation incident upon a solar cell, but let "pass" through the filter optical radiation lying within a spectral band bounded by the excluded IR and UV radiations.

In general a silicon solar cell is operative responsive to radiation of wavelengths between  $0.40\mu\text{m}$  to  $1.10\mu\text{m}$ .

Solar energy outside of this band is generally not converted into electricity and when absorbed only heats up the solar cell thereby reducing its efficiency.

Certain types of optical band-pass filter comprise a multi-layer stack structure arranged upon a substrate, such as a glass substrate. Such multi-layer band-pass filters are designed to reflect IR radiation (or near-IR radiation) that lies immediately adjacent one side of a spectral band of radiation in respect of which a solar cell is intended to operate (e.g.  $0.4\mu\text{m}$  to  $1.1\mu\text{m}$  wavelengths), to transmit optical radiation lying within

that spectral band and to reflect UV lying adjacent the other side of the spectral band of the solar cell.

The band-pass transmission spectra of such multi-layer filters is achieved by forming the stack of layers from repeating pairs of adjacent layers in which any one layer of a pair is comprised of material having an index of refraction which differs from the index of refraction of the other layer of the pair. Thus, the resulting multi-layer stack has an index of refraction which periodically jumps between two values as the depth of the multi-layer stack increases.

As is well known to those skilled in the art, the "optical thickness" of a layer is given by multiplying the physical thickness of the layer by the index of refraction of the material of the layer for a particular wavelength of optical radiation. Thus, a layer of constant physical thickness will have an optical thickness which depends upon the wavelength of optical radiation passing through it.

By appropriately controlling the physical thickness of each of the two layers in the repeated pair of layers such that each has an optical thickness equal to  $\frac{1}{4}$  of a predetermined optical "design" wavelength (e.g. an IR

wavelength), the multi-layer stack causes reflection of optical radiation to occur not only at (and around) the predetermined "design" wavelength, but also at (and around) other wavelengths corresponding to "higher order" frequencies equal to an odd-integer multiple of the "design" frequency. The result is known as a " $\frac{1}{4}$ -wave" stack, or "interference filter".

Thus, such a quarter-wave stack may be employed as an optical filter for reflecting IR radiation by selecting the predetermined wavelength to be a suitable IR wavelength such that a reflection band is formed adjacent a desired spectral pass-band. However, a drawback of such interference filters is that the aforementioned "higher order" reflection bands often reside well within the desired spectral pass-band. Thus, such filters may well reflect radiation which it is not desirable to reflect.

Other types of multi-stack optical interference filter have been proposed in which the multi-layer stack is composed of materials having three different refractive indices rather than just two. By appropriately arranging the three different layer types in a repeating pattern within the stack of layers, the resultant structure is able to suppress the first few of the offending "higher

order" reflection bands which usually occur in simple  $\frac{1}{4}$  - wave stacks as discussed above.

However, a common feature of the simple two-index  $\frac{1}{4}$ -wave stacks and of the aforementioned three-index stacks is the presence of a discontinuity in refractive index as between neighbouring stack layers. This discontinuity arises due to the sudden change in material (and optical properties thereof) at the interface between adjacent stack layers. Such discontinuities are detrimental to the performance and structure of the filter for the following reasons.

The strength of the multi-layer stack is sensitively dependent on the degree of interfacial adhesion between adjacent stack layers. Since adjacent layers in the aforementioned prior art devices are comprised of different materials, it is often the case that the differences (either chemical and/or physical) between such neighbouring layers reduce the strength of the interfacial bond which results in the interface being a primary site of structural weakness in the multi-layer stack.

Furthermore, in existing interference filters such as those described above, the transmission spectrum thereof

at regions in between successive reflection bands are not uniformly transmissive. That is to say, although the reflection bands of such interference filters are generally mainly confined to a limited spectral band, 5 they are in fact not fully so confined. Rather, the so-called reflection "bands" often possess significant ripples or transients of non-zero optical reflectance in the filter at spectral regions within the pass-band thereof.

10

This spreading/dispersion of the reflection band into the pass-band is principally due to the discontinuity in refractive index occurring at the interface of successive layers of a stack. It is detrimental to the transmission 15 spectrum of such filters since it attenuates optical radiation which it is intended to pass to an underlying solar cell. Hence, solar cell efficiency is reduced.

It is an aim of the present invention to overcome at 20 least some of the aforementioned deficiencies in the prior art. It is also an aim of the present invention to permit greater design flexibility when varying the structure of an optical filter in order to optimise its performance.

25

Accordingly, in a first of its aspects, the present invention may provide an optical filter including a substrate having a plurality of layers of materials stacked upon it each of which layers is formed from one or both of:

5 a first material having a first index of refraction; and, a second material having a second index of refraction being less than the first index of refraction; wherein the plurality of layers of materials include a 10 first layer and a second layer each formed from an inhomogeneous mixture of said first material and said second material and a third layer formed from the first material being stacked in between the first layer and the second layer wherein the optical thickness of each of 15 said first and said second layers is greater than the optical thickness of said third layer.

Due to the inhomogeneous mixing of the first material and the second material, when forming the first and second 20 layers, the index of refraction of those layers varies with the depth of the layer between values greater than the second index of refraction and less than the first index of refraction.

25 Thus, by constructing an interference filter in the form of a multi-layer stack (on a substrate) comprising a

repeating group of layers, the group including at least a relatively high refractive index layer sandwiched between two layers of varying (but lower) refractive index, one may for example, provide an interference 5 filter which substantially reduces or suppresses ripples, oscillations or transients of non-zero optical reflectance that would otherwise tend to occur outside the main reflectance band, and "higher order" reflectance bands, of the multi-layer stack. That is to say, the 10 transmission spectrum of the resulting multi-stack filter will tend to vary substantially more monotonically within/across the pass-band of the filter, or if not monotonically then will at least oscillate with lesser amplitudes therein.

15

Furthermore, the present invention is able to reduce or substantially remove any discontinuity in refractive index and material composition/structure as between adjacent layers of a multi-layer stack. Consequently, 20 since a portion of an inhomogeneous layer immediately adjacent a neighbouring layer is materially very similar (or identical) to that neighbouring layer, the bonding of the two layers in question at their interface is enhanced thereby strengthening the multi-layer structure at that 25 interface.

Indeed, it is to be understood that each of the "layers" of the optical filter of the present invention are formed from a particular choice of the proportions of the same two ingredient materials. The term "layer" used herein 5 therefore refers to strata of differing material composition occurring in a continuously formed object whereby each strata corresponds to a particular composition(s) in the material forming the continuous object rather than corresponding merely to the 10 collocation or joining of independent layers.

As will be well known to persons of skill in the art, the "optical thickness" of a layer of material is given by multiplying the physical thickness of the layer by the 15 index of refraction of that layer. For layers of varying refractive index, the optical thickness is given by integrating the depth-dependent refractive index across the depth of the layer in question.

20 Preferably the optical thickness of the first layer and of the second layer each differ in magnitude from a value  $2Q$  by less than  $Q/2$ , and the optical thickness of the third layer differs in magnitude from the value  $Q$  by less than  $Q/2$ , where  $Q$  is the optical thickness of a given 25 said layer traversed by substantially  $\frac{1}{4}$  of a wavelength

of optical radiation of a common reference wavelength at which said optical thicknesses are determined.

It has been found that, starting from a basic design template in which the optical thicknesses of the first, third and second layers of a stack are respectively as follows:  $(2Q, Q, 2Q)$ ; one may optimise the performance of the filter by subsequently varying these three optical thicknesses during design of the filter and prior to its manufacture. This variation is, of course, achieved by varying the physical thickness of the relevant layers such that the associated optical thickness varies from the starting value of the basic design template by any suitable value provided that the variation in the value of the optical thickness is less than  $Q/2$ .

For example, the optical thickness of the first layer may be substantially equal to the optical thickness of the second layer, or the two said layers may differ in optical thickness. In either case, the optical thickness of the first and second layers may or may not be equal in value to  $2Q$  depending upon whether or not design optimisation requires this.

Alternatively, the optical thickness of the first layer and of the second layer may each be substantially equal

to the value  $2Q$ . The optical thickness of the third layer may also be varied when optimising design performance and may be substantially equal to the value  $Q$  or may differ from that value by an amount less than  $Q/2$ .

5

Preferably the optical filter includes, within its plurality of layers, a pair of outer layers each being formed from the first material and between which are stacked the first, second and third layers. This results 10 in a five-layer nest including the first, second and third layers sandwiched between the pair of outer layers.

The optical thickness of each of the outer layers preferably differs in value from the magnitude  $Q$  by less 15 than  $Q/2$ . Thus, the optical thickness of the outer layers themselves may also individually be varied within the aforementioned limits in order to assist in optimising the performance of the filter as a whole. For example, the optical thickness of each one of the pair of 20 outer layers may differ from each other or may substantially equal to each. Where the optical thickness of each of the outer layers is substantially equal, this common optical thickness may be equal to  $Q$  or may differ from  $Q$  (by less than  $Q/2$ ).

It is to be understood that the term "inhomogeneous mixture" in respect of the mixing of materials of differing refractive index, is intended to refer to the nature of the relative proportions of mixed components 5 (which form the mixture) being not homogeneous throughout at least part of the depth of the layer formed by the inhomogeneous mixture. The result of the inhomogeneity of the mixture is a variation of the refractive index of the layer so formed between different depth locations in 10 the same layer.

The index of refraction of the first and/or second layer may vary continuously through at least a part of the depth of the respective layer. Alternatively, or 15 additionally, the index of refraction of the first and/or one second layer may vary substantially in a step-wise manner through at least a part of the depth of the respective layer. In such an arrangement, the first and/or second layer may be a physically continuous 20 article, not being physically discontinuous but having a spatial distribution (inhomogeneous) of mixture which causes sharp/rapid or substantially step-wise changes in the refractive index of the layer at certain regions of depth thereof where the mixture changes correspondingly 25 sharply/rapidly or substantially in a step-wise way (or nearly so).

All variations in the index of refraction of the first and/or second layer may occur sharply/rapidly or substantially in a step-wise manner. In such a case the 5 first and/or second layer may preferably comprise a plurality of sub-regions each of which is formed from a homogeneous mixture of the first material and the second material whereby the homogeneous mixture forming any one sub-region differs from the homogeneous mixture forming 10 immediately neighbouring sub-regions within the intermediate layer such that the index of refraction of each of the plurality of sub-regions is substantially constant through the depth of the sub-region and the index of refraction of the respective first and/or second 15 layer varies sharply/rapidly or substantially step-wise between successive sub-regions thereof.

This amounts to a "digitisation" of the variations in refractive index of the first/second layer. Once more, 20 neighbouring sub-regions of the digitised first/second layer may be physically continuously formed within one physically continuous respective layer. However, by suitably controlling the inhomogeneous mixture of the two materials, one may cause the mixture to change 25 substantially step-wise between neighbouring sub-regions

thereby causing a corresponding "step" in the refractive index therebetween.

In such an arrangement, or in other arrangements, all 5 variations in the index of refraction of the first and/or second layer may increase that index of refraction as the depth of the respective layer increases from regions thereof remote from the third layer to regions thereof proximate the third layer. Thus, for example, one may 10 apply the aforementioned digitisation to a refractive index "ramp", or may have a smoothly varying refractive index ramp.

The plurality of layers are preferably arranged to form a 15 stack of layers in which successive layers are arranged in a periodically repeating order across the depth of the stack.

The filter may be arranged to substantially reflect at 20 least Infra-Red radiation and to transmit optical radiation at least in the visible optical spectrum. The filter may be arranged to substantially reflect at least Infra-Red radiation and Ultra-violet radiation.

25 The present invention may also provide a cover for a photovoltaic cell comprising a filter according to the

first aspect of the invention, and may comprise a photovoltaic cell comprising such a cover. The photovoltaic cell is a preferably solar cell.

5 In a second of its aspects, the present invention may provide an optical filter including a substrate having a layer arranged upon it formed from an inhomogeneous mixture of:

a first material having a first index of refraction;  
10 and,

a second material having a second index of refraction being less than the first index of refraction; the inhomogeneous mixture being such that the value of the index of refraction of the layer oscillates with the 15 depth of the layer between values greater than the second index of refraction and less than the first index of refraction. This may either be an alternative to, or may form a part of, a multi-layer stack type filter. In the former case, the oscillating variations in refractive 20 index result in a filter having one main reflection band (which may be centred on an IR frequency) and has substantially no "higher order" type reflection bands. Since "higher order" reflection bands are suppressed in such a case, the filter is able to operate as an IR 25 filter only with little or substantially no reflection of other wavelengths outside the single reflection band.

The oscillating variations of the value of the index of refraction of the layer, according to the invention in its second aspect, may include at least some sharp/rapid

5. or substantially step-wise variations, or the variations may be mostly (or only) such sharp/rapid or substantially step-wise variations. In such a case the layer may preferably comprise a plurality of sub-regions each of which is formed from a homogeneous mixture of the first

10 material and the second material whereby the homogeneous mixture forming any one sub-region differs from the homogeneous mixture forming immediately neighbouring sub-regions within the layer such that the index of refraction of each of the plurality of sub-regions is

15 substantially constant with the depth of the sub-region and the index of refraction of the layer varies rapidly/sharply or substantially step-wise between successive sub-regions thereof.

20 In this way, the oscillating refractive index of the layer may be a partially, or wholly, "digitised" oscillation (e.g. a digitised wave shape) rather than a continuous oscillation ( e.g. wave) as may be the case alternatively. An optical filter, according to the

25 second aspect of the present invention, may form a filter for a photovoltaic cell such as a solar cell. For

example, a solar cell may be formed having an optical filter comprising only an oscillating (e.g. wave) layer design (digitised or otherwise) according to the present invention in its second aspect. Alternatively, such a

5 wave design could be bounded by other filter layers within a stack of filter layers according to the invention in its first aspect. For example, the wave design may be applied to any one or both of the first and second inhomogeneously mixed layers of the invention in

10 its first aspect. Preferably, the wave design includes a quintic shape comprising one period of a sinusoid oscillation in the refractive index of a given layer across the whole width of the layer.

15 The optical filter, according to either the first or the second aspect of the present invention and any of their aforementioned preferred variants or alternatives, may be for a photovoltaic cell and such as a solar cell.

20 It will be readily appreciated that the present invention, in its first and second aspects and according to any or all of the above variants and preferable features, implements a method of producing an optical filter.

Accordingly, in a third of its aspects, the present invention may provide a method of producing an optical filter, the method including:

providing a substrate;

5 stacking a plurality of layers of materials upon the substrate each of which layers is formed from one or both of:

a first material having a first index of refraction; and, a second material having a second index of refraction

10 being less than the first index of refraction;

forming a first layer and a second layer of the plurality of layers from an inhomogeneous mixture of the first material and the second material;

forming from the first material a third layer of the

15 plurality of layers being stacked between said first and second layers;

wherein the optical thickness of each of said first and second layers is greater than the optical thickness of said third layer.

20

Due to the inhomogeneous mixture of the first material and the second material when forming the first and second layers, the index of refraction of the first and second layer varies with the depth of the intermediate layers 25 between values greater than the second index of refraction and less than the first index of refraction.

According to this method, the first layer and the second layer may each be formed with an optical thickness which differs in magnitude from the value  $2Q$  by less than  $Q/2$  and the third layer may be formed with an optical thickness which differs in magnitude from the value  $Q$  by less than  $Q/2$ , where  $Q$  is the optical thickness of a given layer traversed by substantially  $\frac{1}{4}$  of a wavelength of optical radiation of a common reference wavelength at 5 which the optical thicknesses are determined.

The first layer and second layer may be formed such that the optical thicknesses thereof differ, or such that the optical thicknesses thereof are substantially equal in 10 value. Where the first layer and the second layer are each formed to have an optical thickness of equal value, this value may be substantially equal to  $2Q$ , or may be equal to some other value differing from  $2Q$  by less than  $Q/2$ . The third layer may be formed to have an optical 15 thickness substantially equal to  $Q$ .

The method may include the step of forming a pair of outerlayers, being part of the plurality of layers, each being formed from the second material wherein the outer 20 layers are formed with the first, second and third layers 25 being stacked between them. The pair of outer layers may

be formed such that the optical thickness of each such layer differs in value from the magnitude  $Q$  by less than  $Q/2$ . The optical thicknesses of each of the pair of outer layers may be substantially equal to each other, 5 and may also be substantially equal to the value  $Q$ .

It is to be appreciated that variations in the optical thickness of one, some or all of the layers of the optical filter (including the first, second, third and 10 outer layers) may be varied for the purposes of optimising the performance of the resultant filter. Consequently, the method, according to the invention in its third aspect, may include varying the optical thickness of one, some or all of the layers in said 15 plurality of layers for the purpose of optimising the spectral response of the optical filter for: transmitting solar radiation within a band of wavelengths to which a solar cell is operatively designed to be sensitive to, and, for reflecting solar radiation outwith said band.

According to this method the first and/or second layer may be formed such that the index of refraction thereof varies continuously through at least a part of the depth of the respective layer.

Alternatively, or additionally the first and/or second may be formed such that index of refraction thereof varies substantially in a step-wise manner through at least a part of the depth of the respective layer.

5

- The first and/or second layer may be formed such that all variations in the index of refraction thereof occur substantially in a step-wise manner.
- 10 The first and/or second layer may be formed to comprise a plurality of sub-regions each of which is formed from a homogeneous mixture of the first material and the second material whereby the homogeneous mixture forming any one sub-region differs from the homogeneous mixture forming 15 immediately neighbouring sub-region within the first and/or second layer such that the index of refraction of each of the plurality of sub-regions is substantially constant with the depth of the sub-region and the index of refraction of the first and/or second layer varies 20 substantially step-wise with depth between successive sub-regions thereof.

The first and/or second layer may be formed such that all variations in the index of refraction of the respective 25 layer increase that index of refraction as the depth of

the layer increases from regions thereof remote from the third layer to regions thereof proximate the third layer.

The plurality of layers are preferably arranged to form a  
5 stack of layers in which successive layers are arranged in a periodically repeating order across the depth of the stack.

The plurality of layers are preferably arranged to  
10 substantially reflect at least Infra-Red radiation and to transmit optical radiation at least in the visible optical spectrum.

The plurality of layers may be arranged to substantially  
15 reflect at least Infra-Red radiation and Ultra-violet radiation.

Non-limiting examples of the present invention shall now be described with reference to the accompanying drawings  
20 in which:

Figure 1 illustrates a transmission spectrum for a simple  $\frac{1}{4}$ -wave interference-type multi-stack optical filter, the spectrum comprising a main reflection band, and a "higher order" reflection band, and reflectance  
25 ripples/oscillations in between;

Figures 2a, 2b and 2c illustrate the variation in refractive index of a part of a multi-layer stack of an optical filter;

Figure 3 illustrates a transmission spectrum for an 5 interference-type multi-layer stack optical filter employing multi-layer stacks of the form illustrated in Figures 2a, 2b or 2c;

Figure 4 illustrates a multi-layer optical filter comprising a stacked plurality of layer nests each nest 10 being a multi-layer stack of the type illustrated in Figures 2a, 2b or 2c.

Referring to Figure 1 there is illustrated a typical optical transmission spectrum 1 for a simple 15 interference-type (or  $\frac{1}{4}$ -wave type) multi-layer stack optical filter of known type comprising a stack of layers of alternate high and low refractive index each layer being of an optical thickness equal to  $\frac{1}{4}$  where  $\lambda_0$  is a specified "design" wavelength (e.g.  $\lambda_0 = 1250\text{nm}$ ) . The 20 spectrum illustrates the variation in the optical transmission coefficient (T) of the filter as a function of incident optical radiation wavelength ( $\lambda$ ) across a spectral region encompassing the operating bandwidth of a typical solar cell (e.g. from about 400 nm to about 1100 25 nm in optical wavelength).

The transmission spectrum 1 has a main broad reflection band 2 (i.e. low or zero transmission) centred at an optical wavelength of 1250 nm within the IR region of the optical spectrum, and a relatively narrow "higher order" reflection band 3 centred at an optical wavelength of 417 nm (i.e.  $417 = 1250/3$  approx.) within the blue/violet region of the optical spectrum and within the operating bandwidth of the solar cell. This "higher order" reflection band is the "third order" reflection band, the "second order" band (at  $\lambda = 625\text{mm} = 1250/2$ ) being suppressed and the "first order" band (at  $\lambda = 1250\text{nm} = 1250/1$ ) being present. A "fourth order" reflection band (at  $\lambda = 312.5\text{nm} = 1250/4$ ) is also suppressed.

The transmission spectrum 1 also possesses a series of optical transmission transients 4 occurring in between the main "first order" reflection band 2 and the "third order" reflection band 3, and beyond. These optical transmission transients 4 cause the transmission coefficient (T) of the optical filter to repeatedly fall significantly within the operating bandwidth of the solar cell. Both the third order reflection band 3 and the transmission transients 4 are undesirable since they exclude from use optical radiation which it is intended that the solar cell receives.

Figure 4 illustrates an interference-type multi-layer stack optical filter structure according to the present invention. The multi-layer optical filter comprises a multi-layer stack 50 arranged upon a CMG glass substrate 5 about 100 $\mu$ m thick. The multi-layer stack 50 comprises a series of repeating layer groups (or "nests") each of which "nests" comprises a first and outer layer formed from a material (L) having a low refractive index (n). A succeeding second layer is formed from an inhomogeneous mixture (M) of the low-index material (L) and a different material (H) of a relatively high index of refraction. The second layer has a refractive index (n) which varies with the layer's depth this being achieved by the inhomogeneity (with layer depth) of the mixture (M) of the two materials (L and H) forming the layer. A succeeding third layer is formed from the high-index material (H) used in part to form the second layer. A succeeding fourth layer is formed from an inhomogeneous mixture (M) of the low-index material (L) and the height index material (H) such that the refractive index of the fourth layer varies with the depth thereof as a result of inhomogeneous mixing of H and L materials. A final fifth and outer layer is formed from the same material (L) used to form the first layer.

Thus, the refractive index profile of the five-layer "nest" of the stack 50 may be summarised as LMHML as indicated by the "1<sup>st</sup> nest" of Figure 4. Each one of the first, third and fifth layers in the nest has an

5. "optical" thickness of  $\frac{1}{4}$ -wavelength of a predetermined design wavelength (e.g.  $\lambda_0 = 340\text{nm}$ ). That is to say, when optical radiation of the predetermined design wavelength ( $\lambda_0$ ) is propagating through any given one of the first,

10. third or fifth layers within the nest, the wavelength of the radiation within that layer (which may differ from its wavelength as measured in a vacuum) is substantially four times greater than the layer thickness.

Conversely, each one of the second and fourth layers in

15. the nest has an optical thickness of  $\frac{1}{2}$ -wavelength of the predetermined design wavelength. Consequently, when optical radiation of the predetermined design wavelength ( $\lambda_0$ ) is propagating through any given one of the second or fourth layers within the nest, the wavelength of the

20. radiation within that layer is substantially two times greater than the layer thickness.

The "2<sup>nd</sup> nest", and all successive nests, in the stack 50 merely repeat the layering structure of the "1<sup>st</sup> nest".

25. In this example seven nests are stacked upon each other, but fewer or more nests may be so stacked.

Figure 2 illustrates the refractive index profile of any one of the multiple five-layer nests illustrated in Figure 4. The first and fifth layers (the outer layers) 5 each have the same refractive index, 20 and 24 respectively, which is low (L) and homogeneous across the depth of the respective layer. The third layer has a refractive index, 22, which is high (H) and homogeneous across the depth of the layer.

10 Intermediate the first and third layer, and intermediate the third and fifth layers are the second and fourth layers formed of an inhomogeneous mixture of the materials used to form the first, third and the fifth 15 layers, (20, 22 and 24 respectively). The inhomogeneous mixture of the two materials (L and H) in question results in a refractive index (21, 23) for the second and fourth layers respectively which varies continuously with the depth of the respective layer from the lower 20 refractive index value (L), through continuously changing intermediate values to the higher refractive index value (H), the changing intermediate values being between the low value (L) associated with the first or fifth layer and the high value (H) associated with the third layer. 25 The inhomogeneous second or fourth layer thus has a ramped refractive index which increases in value from

regions thereof remote from the third layer to regions thereof proximate the third layer.

In terms of material types, the five-layer nest structure  
5 may be summarised as: (LMHML). However, in terms of  
layer optical thicknesses the five-layer nest may be  
referred to as follows:  $(Q, 2Q; Q, 2Q, Q)^n$ , where Q  
refers to  $\frac{1}{4}$ -wavelength of the predetermined design  
wavelength (e.g.  $\lambda_0 = 340\text{nm}$ ). The integer "n" refers to  
10 the number of times that the nest layer may be repeated  
in the optical stack design, in this example  $n = 7$ .

It is to be noted that the optical thicknesses of  
successive layers illustrated in the designs of Figures  
15 2a, 2b and 2c correspond with what may be termed a  
"template" or basic design arrangement which may  
subsequently be optimised by varying the optical  
thickness of one, some or all of the optical layers in  
one, some or all of the nests within a complete optical  
20 filter. It has been found that by varying the optical  
thickness of individual layers, or by varying layer  
optical thicknesses collectively, one may optimise the  
spectral response of the optical filter for the purposes  
of transmitting solar radiation within a band of  
25 wavelengths to which, for example, a solar cell is

operatively designed to be sensitive to, and, for optimally reflecting solar radiation outwith that band.

It has been found that provided that the optical  
5 thickness of each of the second and fourth layers (being  
the inhomogeneously mixed layers) exceeds the optical  
thickness of the third (high-index) layer, and where  
present the outer (low-index) layers, by less than  $\frac{1}{8}$  of  
the design wavelength (i.e. by less than  $\lambda_0/8$ ) then a  
10 suitable spectral response can be achieved in the optical  
filter.

Referring to Figure 3 there is illustrated a transmission  
spectrum for a multi-stack optical filter comprising  
15 seven stacked five-layer nests of the form (Q, 2Q, Q, 2Q,  
Q)<sup>7</sup>, each nest having a five-layer refractive index  
distribution of the form (LMHML) as illustrated in Figure  
2a, 2b or 2c. The spectrum of Figure 3 comprises a main  
20 "first order" reflection band centred at a wavelength of  
1250nm and a fourth-order reflection band centred at a  
wavelength of 312.5nm (i.e.  $312.5 = 1250/4$ ). It is to be  
noted that the region of the transmission spectrum  
intermediate the first order and fourth order reflection  
bands enjoys a high level of transmittance in which the  
25 presence of transmittance transients 32 is significantly  
suppressed. Furthermore, not only is the second-order

reflection band completely suppressed at a wavelength of 625nm (i.e.  $625 = 1250/2$ ), but also the third-order reflection band 3 centred at 417nm (i.e.  $417 = 1250/3$ ) is suppressed. This is to be compared with Figure 1 in 5 which simple  $\frac{1}{4}$ -wave stacks are unable to suppress the third-order reflection band at 417nm.

The basic transmission spectrum illustrated in Figure 3 may be further improved by suitably optimising the design 10 parameters employed in each of the seven nests of the optical filter with which the spectrum is associated. As mentioned above, this may involve suitable variations in the optical thicknesses of one, some or all of the five layers within each nest. For example, in terms of 15 optical thicknesses, a nest may be modified to: (1.1Q, 2.3Q, 1.1Q, 2.3Q, 1.1Q). This variation is just one illustrative example of how relative thicknesses may be varied, and different variations may be applied to different nests in the multi-layer stack.

20

Furthermore, the gradient of the refractive index (i.e. the variation of refractive index as a function of layer depth) of one or both of the second and fourth inhomogeneously mixed layers of a given nest may also be 25 varied in the procedure for optimising the spectral response of the filter. An example of this is shown in

Figure 2b wherein the second layer 25 and the fourth layer 26 each display a variation in refractive index which is reduced relative to that illustrated in Figure 2a. In this example each of the inhomogeneously mixed 5 layers is formed such that the refractive index of the layer varies from a lower intermediate value ( $M_1$ ) which is greater in value than the low refractive index value associated with the first layer 20, to a second intermediate value ( $M_2$ ) greater than the first 10 intermediate value ( $M_1$ ) but less than the high-index value associated with the third layer.

Indeed, it has been found that the mere presence of a distinctive ramping in the refractive indices of the 15 second and fourth layer towards the third layer is sufficient to provide good optimisation of the spectral response of a filter, while the specifics of each ramp shape may subsequently be optimised to "fine-tune" the spectral response.

20 The form of the refractive index ramp in the second and/or fourth layers need not be linear, and may be exponentially increasing (as towards the third layer) or may be some other more complex ramp shape. Indeed, a 25 quintic ramp shape may be employed in which the refractive index of either the second or fourth layer is

formed so as to gently oscillate over a single sinusoid period, the quintic oscillation being superimposed upon an underlying ramp increase in the refractive index.

5 Figure 2c illustrates a further design variant of the embodiments described herein, and shows the refractive index (n) variations of the inhomogeneously mixed second and fourth layers (27, 28) which vary substantially in a step-wise manner through the depth of the respective 10 layer. In this arrangement, the second and fourth layer (27, 28) are each physically continuous articles, not being physically discontinuous but having a spatial distribution (inhomogeneous) of mixture (M) which causes substantially step-wise changes in the refractive index 15 of the respective layer at certain sub-regions thereof where the mixture changes correspondingly substantially step-wise (or nearly so).

In this variant, the second/fourth layer comprises a 20 plurality of sub-regions, such as sub-layers 65 and 70 of Figure 2c, each of which is formed from a homogeneous mixture of the first material (L) and the second material (H) over a thickness "x" of the layer. The homogeneous mixture forming any one sub-region differs from the 25 homogeneous mixture forming immediately neighbouring sub-region within the second/fourth layer (M) such that the

index of refraction of each of the plurality of sub-regions is substantially constant with the depth "x" of the sub-region. However, the index of refraction of the second/fourth layer (M) varies substantially step-wise 5 between successive sub-regions thereof. This amounts to a full "digitisation" of the variations in refractive index of the second and fourth layer.

Once more, it is to be noted that the neighbouring sub-regions of the digitised second/fourth layers are physically continuously formed within one physically continuous respective layer and do not represent 10 separately formed sub-layers. However, by suitably controlling the inhomogeneous mixture of the two 15 materials (L & H), one may cause the mixture to change substantially step-wise between neighbouring sub-regions thereby causing a corresponding "step" in the refractive index therebetween.

20 The "digitised" inhomogeneous refractive index profile illustrated in Figure 2c may be applied in place of (or in addition to) the smoothly varying index ramps of the second and fourth layers of Figures 2a and 2b. Indeed, this has been found to be easier to achieve than a 25 smoothly varying varying refractive index ramp.

An advantage of such digitisation is that the formation of such digitised shapes requires less control in the apparatus used to inhomogeneously mix the two differing materials employed in the mixture. The need to 5 continuously regulate/vary the mixture is obviated when digitisation is employed.

Materials which may be employed in forming the layers of a multi-layer stack 50 of an optical filter (50, 60) 10 according to the present invention include Silicon dioxide ( $\text{SiO}_2$  and Hafnium dioxide ( $\text{HF}_2\text{O}$ )), and a substrate glass 60 such as CMG glass.

For example, the following table illustrates an example 15 of the physical thicknesses of each of the five layers in a given five-layer nest employed in a multi-nest stack. The outer first and fifth layers are each formed from Silicon dioxide, and the third high index layer is formed from Hafnium dioxide, while the second and fourth 20 intermediate-index layers are formed from an inhomogeneous mixture of Silicon dioxide and Hafnium dioxide. The physical layer thicknesses indicated in the table below may be translated into optical thicknesses by multiplying the physical thickness with the refractive 25 index of the material of the respective layer for the design wavelength of this example which is  $\lambda_0 = 340$  nm.

The refractive indices at the design wavelength are as follows:

$\text{SiO}_2$  - 1.46;

$\text{HfO}_2$  - 2.09.

5 This gives physical thicknesses for the unmixed layers as:

$\text{SiO}_2$  - 58.2nm;

$\text{HfO}_2$  - 40.6nm,

for a design wavelength of 340nm. The physical thickness 10 of each ramped layer (layers 2 and 4) of inhomogeneously mixed materials  $\text{SiO}_2$  &  $\text{HfO}_2$  is 95.7nm and in this example the refractive index of each of the two mixed layers (layers 2 and 4) ramps linearly from an index of 1.46 (adjacent an outer layer 1 or 5) to and index of 2.09 15 (adjacent the high index layer 3).

<u>Layer</u>	<u>Material</u>	<u>Layer thickness(physical) nm</u>
0	CMG GLASS	-
20 1	$\text{SiO}_2$	58.2
2	$\text{SiO}_2$ & $\text{HfO}_2$	95.7
3	$\text{HfO}_2$	40.6
4	$\text{SiO}_2$ & $\text{HfO}_2$	95.7
5	$\text{SiO}_2$	58.2

The above embodiments are intended to be examples of the present invention and variants and modifications of those

embodiments, such as would be readily apparent to the skilled person, are envisaged and may be made without departing from the scope of the present invention.

Claims:

1. An optical filter including a substrate having a plurality of layers of materials stacked upon it each of which layers is formed from one or both of:
  - 5 a first material having a first index of refraction;
  - and,
  - 10 a second material having a second index of refraction being less than the first index of refraction;wherein the plurality of layers of materials include a first layer and a second layer each formed from an inhomogeneous mixture of said first material and said second material; and a third layer formed from the first material being stacked in between the first layer and the second layer;wherein the optical thickness of each of said first and said second layers is greater than the optical thickness of said third layer.
- 20 2. An optical filter according to Claim 1 wherein the optical thickness of said first layer and of said second layer each differ in magnitude from the value  $2Q$  by less than  $Q/2$ , and the optical thickness of said third layer differs in magnitude from the value  $Q$  by less than  $Q/2$ , where  $Q$  is the thickness of a

given said layer traversed by substantially one quarter of a wavelength of optical radiation of a common reference wavelength at which said optical thicknesses are determined.

5

3. An optical filter according to Claim 1 or Claim 2 wherein the optical thickness of said first layer is substantially equal to the optical thickness of said second layer.

10

4. An optical filter according to Claim 2 wherein the optical thickness of said first layer and of said second layer are each substantially equal to  $2Q$ , and the optical thickness of said third layer is substantially equal to  $Q$ .

15

5. An optical filter according to any of preceding claims 2 to 4 wherein said plurality of layers of materials include a pair of outer layers each being formed from said second material and between which are stacked said first, second and third layers.

20

6. An optical filter according to Claim 5 wherein the optical thickness of each of said pair of outer layers differs in value from the magnitude  $Q$  by less than  $Q/2$ .

25

7. An optical filter according to Claim 5 or 6 wherein the optical thickness of each one of the pair of outer layers is substantially equal to the optical thickness of the other of the pair.  
5
8. An optical filter according to Claim 7 wherein the optical thickness of each of the outer layers is substantially equal to Q.  
10
9. An optical filter according to any preceding claim wherein the index of refraction of the first and/or second layer varies continuously through at least a part of the depth of the respective layer.  
15
10. An optical filter according to any preceding claim wherein the index of refraction of the first and/or second layer varies substantially in a step-wise manner through at least a part of the depth of the respective layer.  
20
11. An optical filter according to any of preceding claims 1 to 8 and 10 wherein all variations in the index of refraction of the first and/or second layer occur substantially in a step-wise manner.  
25

12. An optical filter according to Claim 10 or Claim 11 wherein the first and/or second layer comprises a plurality of sub-regions stacked therein each of which is formed from a homogeneous mixture of the first material and the second material whereby the homogeneous mixture forming any one sub-region differs from the homogeneous mixture forming immediately neighbouring sub-region(s) within the first and/or second layer such that the index of refraction of each of the plurality of sub-regions is substantially constant with the depth of the sub-regions and the index of refraction of the first and/or second layer varies substantially step-wise with depth between successive sub-regions thereof.

13. An optical filter according to any preceding claim wherein all variations in the index of refraction of the first and second layer increase that index of refraction as the depth of the respective layer increases from regions thereof remote from said third layer to regions thereof proximate the third layer.

14. An optical filter according to any preceding claim in which the plurality of layers form a stack of layers in which successive layers are arranged in a

periodically repeating order across the depth of the stack.

15. An optical filter according to any preceding claim  
5 wherein the filter is arranged to substantially reflect at least Infra-Red radiation and to transmit optical radiation at least in the visible optical spectrum.
- 10 16. An optical filter according to Claim 15 wherein the filter is arranged to substantially reflect at least Infra-Red radiation and Ultra-violet radiation.
- 15 17. A cover for a photovoltaic cell comprising a filter according to any preceding claim.
18. A photovoltaic cell comprising a cover according to Claim 17.
- 20 19. A photovoltaic cell according to Claim 18 wherein the photovoltaic cell is a solar cell.
20. A method of producing an optical filter for use with a photovoltaic cell, the method including:  
25 providing a substrate;

stacking a plurality of layers of materials upon the substrate each of which layers is formed from one or both of:

5 a first material having a first index of refraction; and,

a second material having a second index of refraction being less than the first index of refraction;

10 forming a first layer and a second layer of the plurality of layers from an inhomogeneous mixture of the first material and the second material;

forming from the first material a third layer of the plurality of layers being stacked between said first and second layers;

15 wherein the optical thickness of each of said first and second layers is greater than the optical thickness of said third layer.

21. A method of producing an optical filter according to

20 Claim 20 wherein said first layer and said second layer are each formed with an optical thickness

which differs in magnitude from the value  $2Q$  by less than  $Q/2$ , and said third layer is formed with an optical thickness which differs in magnitude from

25 the value  $Q$  by less than  $Q/2$ , where  $Q$  is the thickness of a given said layer traversed by

substantially one quarter of a wavelength of optical radiation of a common reference wavelength at which said optical thicknesses are determined.

5 22. A method of producing an optical filter according to Claim 20 or Claim 21 wherein the optical thickness of said first layer is formed to be substantially equal to the optical thickness of said second layer and vice versa.

10

23. A method of producing an optical filter according to Claim 21 wherein said first layer and said second layer are each formed to have an optical thickness substantially equal to  $2Q$ , and said third layer is formed to have an optical thickness substantially equal to  $Q$ .

15

24. A method of producing an optical filter according to any of claims 21 to 23 further including the step of forming a pair of outer layers of the plurality of layers each being formed from said second material and between which are stacked said first, second and third layers.

20  
25 25. A method of producing an optical filter according to Claim 24 wherein said pair of outer layers are

formed such that the optical thickness of each differs in value from the magnitude  $Q$  by less than  $Q/2$ .

5 26. A method of producing an optical filter according to Claim 24 or Claim 25 wherein each of said pair of outer layers is formed such that any one such layer has an optical thickness substantially equal to that of the other such layer.

10

27. A method of producing an optical filter according to Claim 26 wherein each layer of the pair of outer layers is formed with an optical thickness substantially equal to  $Q$ .

15

28. A method of producing an optical filter according to any of claims 20 to Claim 27 wherein the first and/or second layer is formed such that the index of refraction thereof varies continuously through at least a part of the depth of the respective layer.

20

29. A method of producing an optical filter according to Claim 28, wherein the first and/or second layer is formed such that index of refraction thereof varies substantially in a step-wise manner through at least a part of the depth of the respective layer.

25

30. A method of producing an optical filter according to any of preceding claims 20 to 27 and 29 wherein the first and/or second layer is formed such that all variations in the index of refraction thereof occur substantially in a step-wise manner.

5

31. A method of producing an optical filter according to Claim 29 or Claim 30 wherein the first and/or second layer is formed to comprise a plurality of sub-regions stacked therein each of which is formed from a homogeneous mixture of the first material and the second material whereby the homogeneous mixture forming any one sub-region differs from the homogeneous mixture forming immediately neighbouring sub-region(s) within the first and/or second layer such that the index of refraction of each of the plurality of sub-regions is substantially constant with the depth of the sub-regions and the index of refraction of the first and/or second layer varies substantially step-wise with depth between successive sub-regions thereof.

10

15

20

25

32. A method of producing an optical filter according to any of preceding claims 20 to 31 wherein the first and/or second layer is formed such that all

variations in the index of refraction of the first and/or second layer increase that index of refraction as the depth of the respective layer increases from regions thereof remote from said third layer to regions thereof proximate the third layer.

5 33. A method of producing an optical filter according to any of preceding claims 20 to 32 wherein the method 10 includes forming the plurality of layers into a stack of layers in which successive layers are arranged in a periodically repeating order across the depth of the stack.

15 34. A method of producing an optical filter according to any of preceding claims 20 to 33 wherein the plurality of layers are arranged to substantially reflect at least Infra-Red radiation and to transmit optical radiation at least in the visible optical 20 spectrum.

25 35. A method of producing an optical filter according to Claim 34 wherein the plurality of layers are arranged to substantially reflect at least Infra-Red radiation and Ultra-violet radiation.

36. A method of optical filtering of radiation incident thereon upon a photovoltaic cell, the method including;

5 producing an optical filter according to any of preceding claims 20 to 35; and,

permitting incident radiation to pass through the plurality of layers so formed.

37. A method of producing an optical filter according to any of claims 20 to 35 including varying the optical thickness of one, some or all of the layers in said plurality of layers for the purpose of optimising the spectral response of the optical filter for: transmitting solar radiation within a band of 15 wavelengths to which a solar cell is operatively designed to be sensitive to; and, for reflecting solar radiation outwith said band.

38. An optical filter substantially as described in any 20 one embodiment hereinbefore with reference to Figures 2a, 2b, 2c, 3 or 4 of the accompanying drawings.

39. A method of producing an optical filter 25 substantially as described in any one embodiment

hereinbefore with reference to Figures 2a, 2b, 2c, 3  
or 4 of the accompanying drawings.

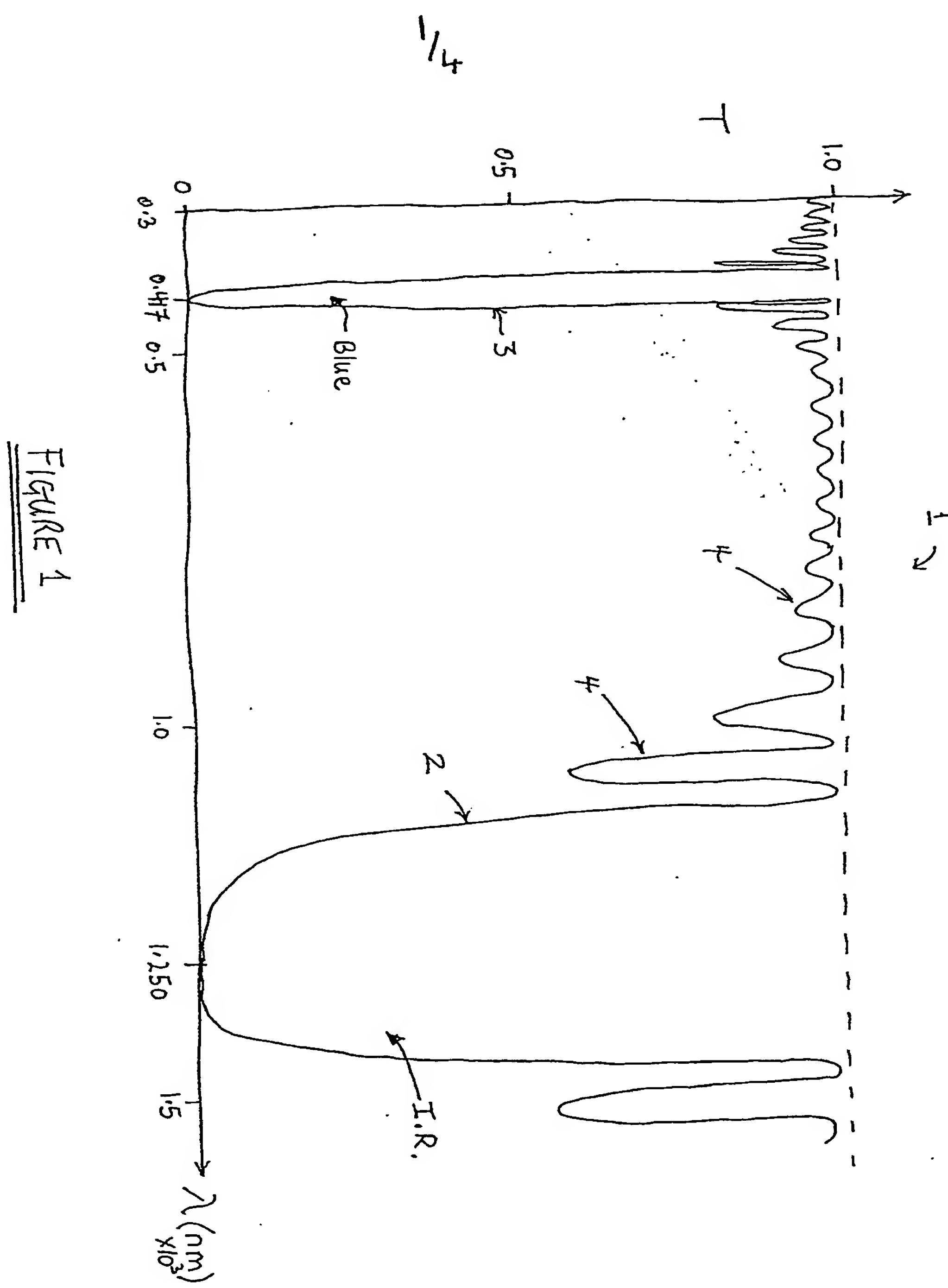


FIGURE 1

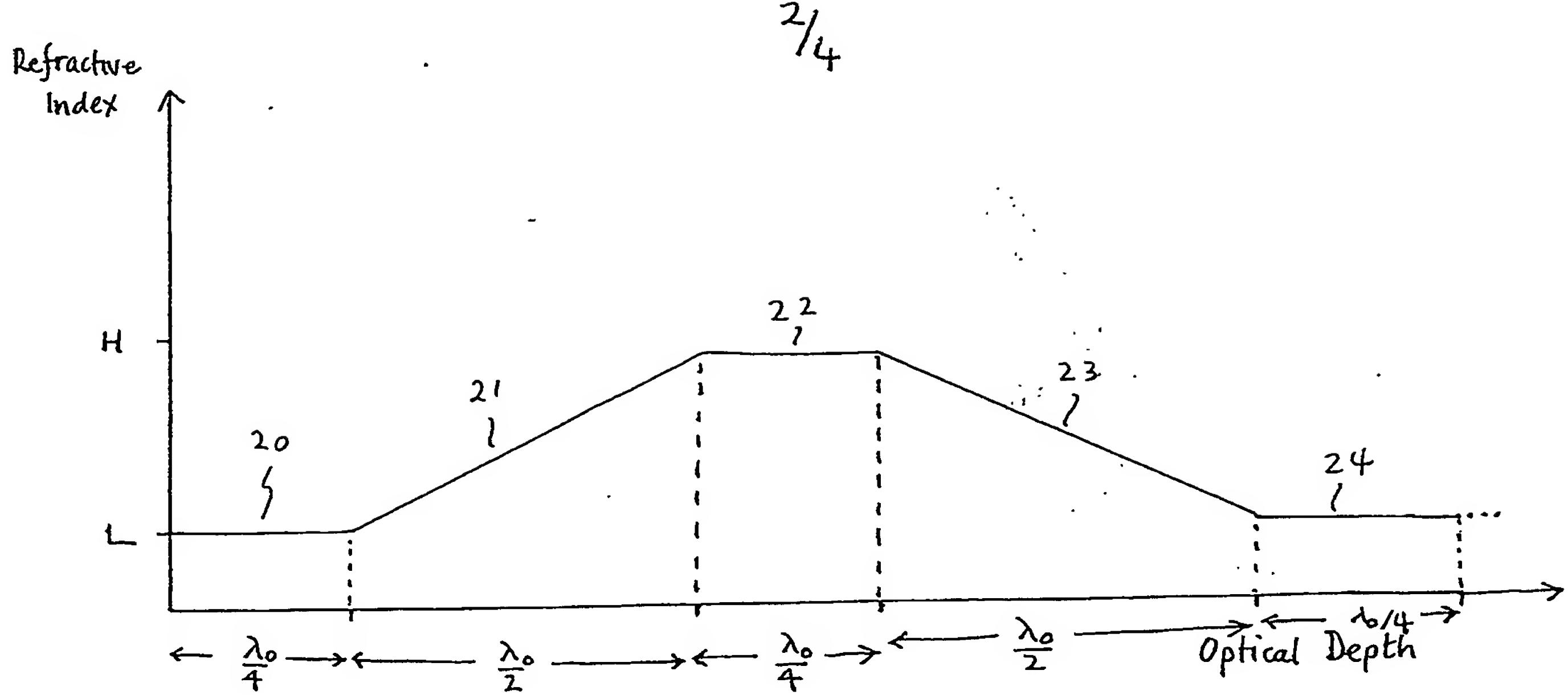


Figure 2a

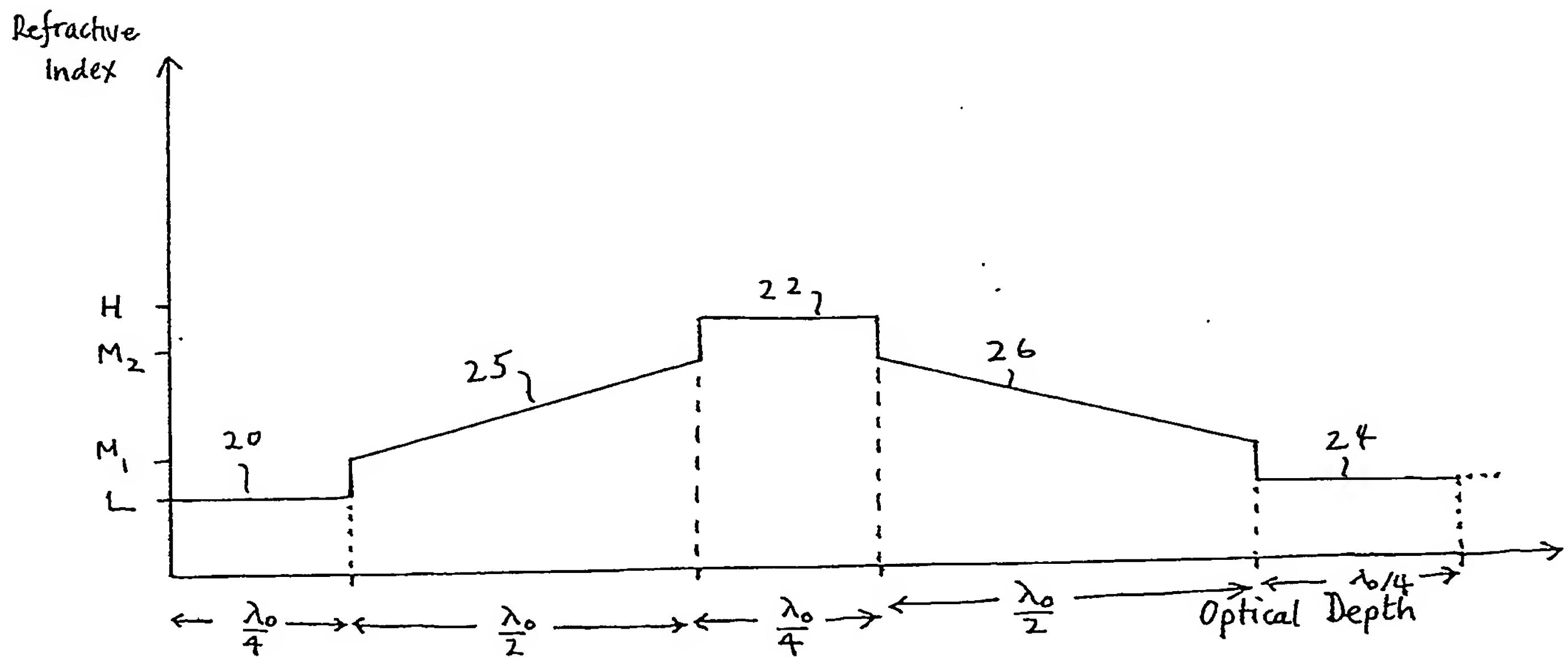
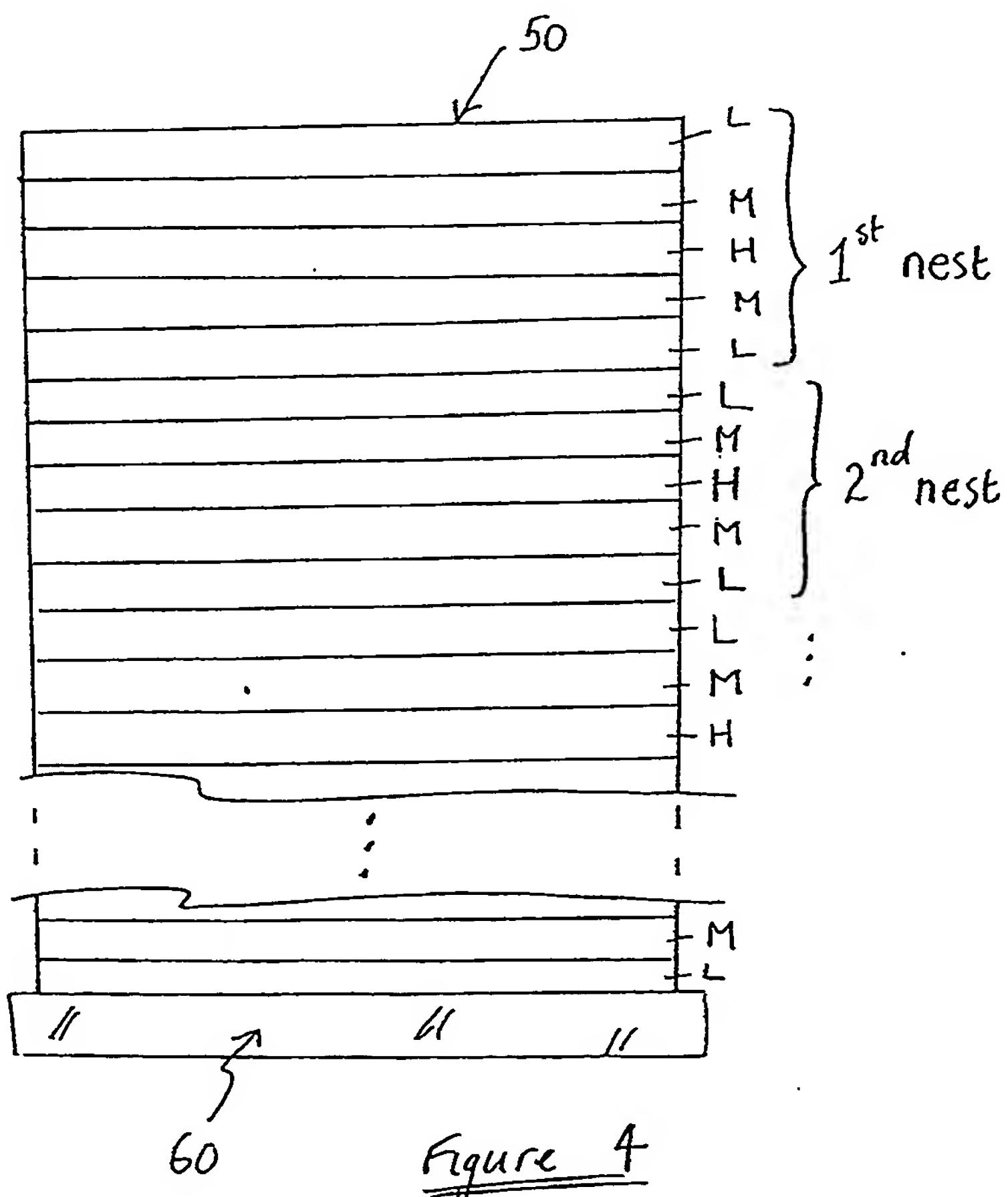
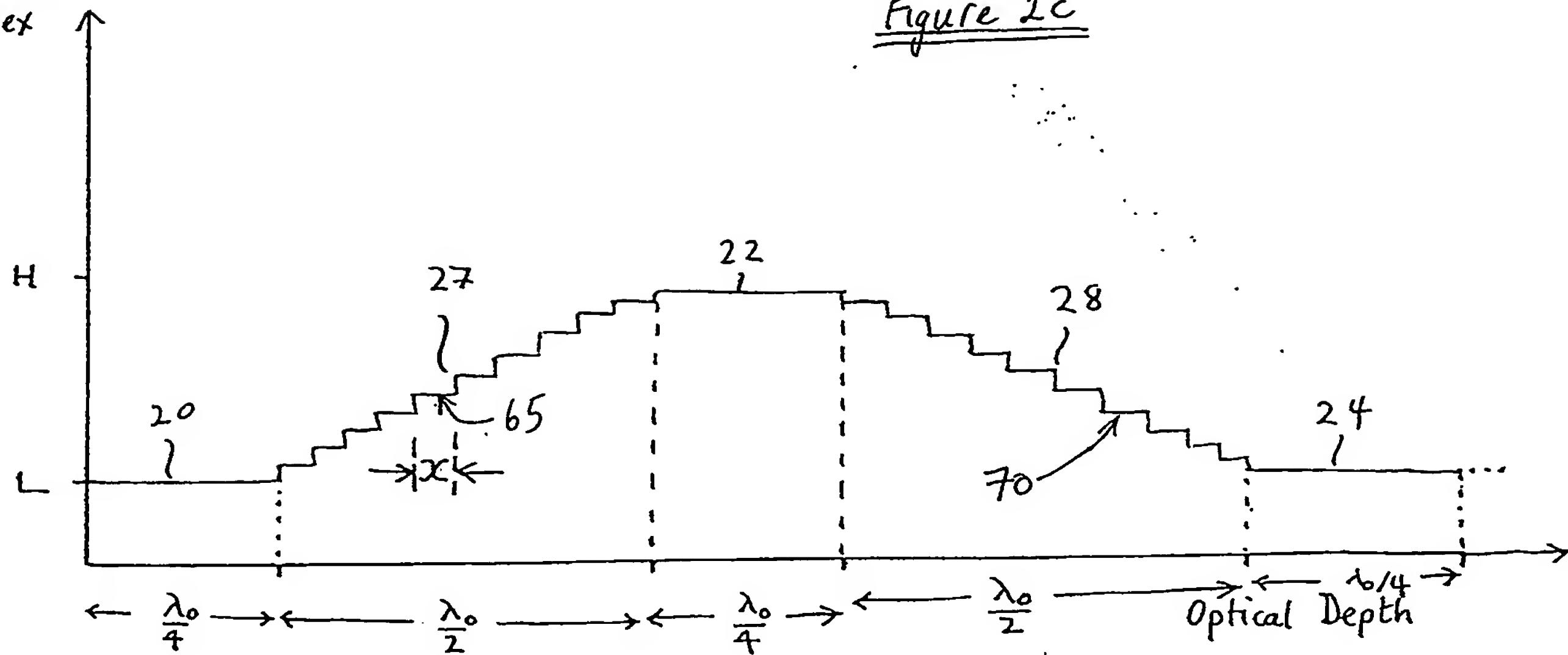


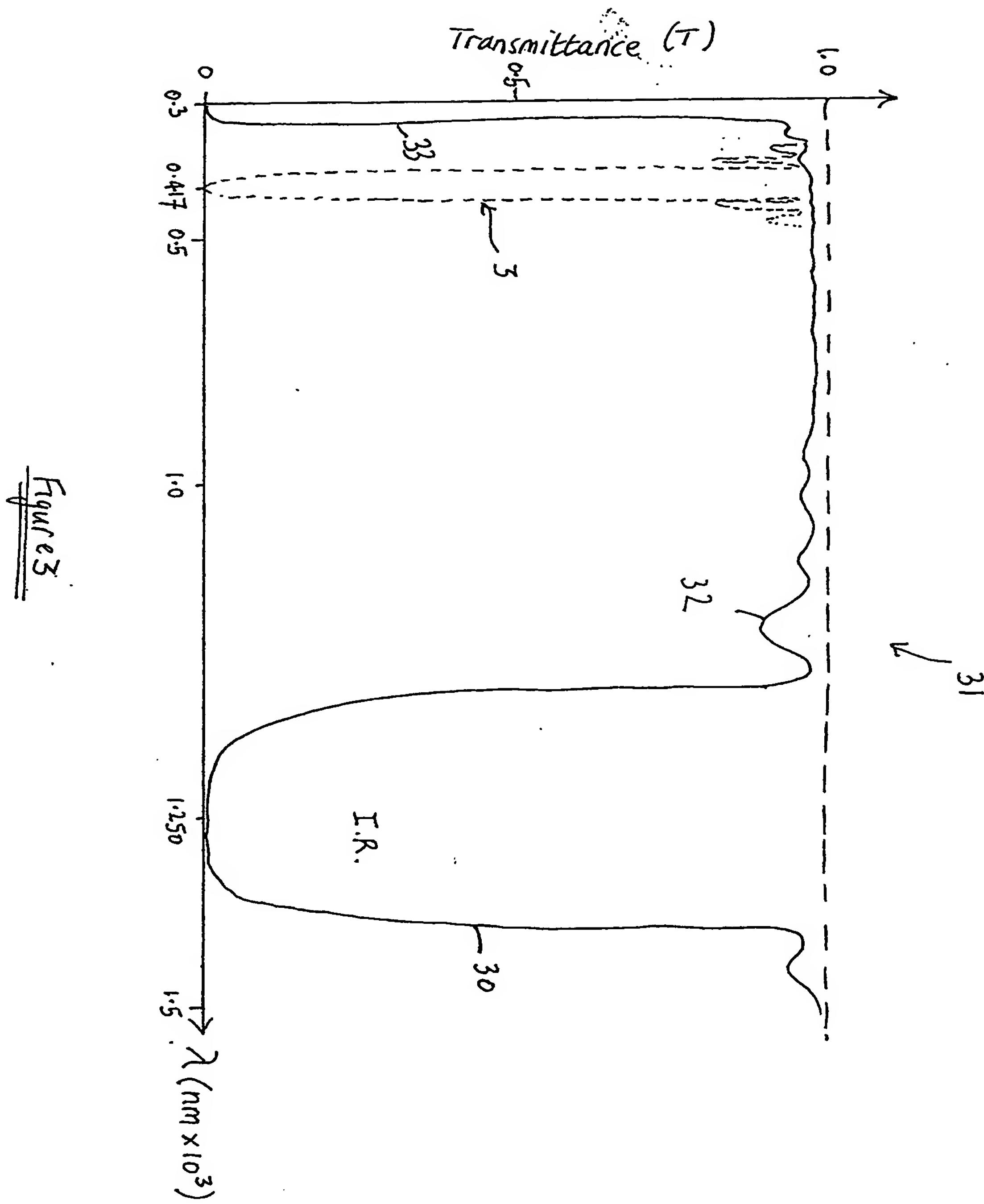
Figure 2b

3/4

Refractive  
Index



4/4



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